CUSTOMIZING INDOOR WIRELESS COVERAGE VIA 3D-FABRICATED REFLECTORS

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Abstract

Judicious control of indoor wireless coverage is crucial in built environments. It enhances signal reception, reduces harmful interference, and raises the barrier for malicious attackers. Existing methods are either costly, vulnerable to attacks, or hard to configure. We present a low-cost, secure, and easy-to-configure approach that uses an easily-accessible, 3D-fabricated reflector to customize wireless coverage. With input on coarse-grained environment setting and preferred coverage (e.g., areas with signals to be strengthened or weakened), the system computes an optimized reflector shape tailored to the given environment. The user simply 3D prints the reflector and places it around a Wi-Fi access point to realize the target coverage. We conduct experiments to examine the efficacy and limits of optimized reflectors in different indoor settings. Results show that optimized reflectors coexist with a variety of Wi-Fi APs and correctly weaken or enhance signals in target areas by up to 10 or 6 dB, resulting to throughput changes by up to -63.3% or 55.1%.
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Chapter 1

Introduction

1.1 Motivation

From residential spaces to commercial real estates, wireless access points (AP) are essential for providing ubiquitous connectivity to mobile devices. As much as we enjoy the wide wireless coverage, we also face two fundamental problems brought by the broadcast nature of APs. First, when multiple APs transmit in the same frequency channel in an uncoordinated manner, signal interference among APs can drastically degrade communication quality. The problem is worsening with the increasing broadband penetration and the widespread uncoordinated deployment of APs. Second, wireless transmissions are vulnerable to security/privacy attacks such as traffic eavesdropping. Even when the transmission is encrypted, an attacker can still obtain network information (e.g., received signal strength) and thereby physically locate the AP or launch other attacks.

Addressing these problems demands active, judicious control of each AP’s wireless coverage in the environment, which improves the efficiency of wireless infrastructure in buildings by mitigating the impact of building’s insulations, partitions, and interior layouts. If we can control the propagation of the electromagnetic waves from an AP (e.g.,
Wi-Fi router), we can better plan the coverage regions of multiple APs. By regulating the physical coverage of each wireless access point (AP), we can enhance signal reception in desired regions while weakening signals in others to reduce harmful interference. In addition, this level of signal steering should be taken as a light-weight access control that enhances the system security and strengthens user privacy. It will not defeat sophisticated attackers with high-end antennas. Rather, it serves as a complimentary method to existing network security measures, such as encryption, and hence raises the barrier for attackers.

1.2 Challenges

Achieving this goal is particularly challenging indoors, because of the complex interactions of radio signals with the environment. Existing approaches rely on directional antennas to concentrate signals in desired directions. These approaches, however, have three shortcomings. First, they face a tradeoff between cost and control flexibility. Low-cost directional antennas (5) concentrate signals in a static direction, offering very few coverage shapes. Antenna arrays with more sophisticated control (e.g., arbitrary beam patterns, dynamic configuration) are costly, e.g., $5000+ for Phocus array (29), $200 for an 802.11ac AP (40). It is because forming a narrow beam needs a large number of antennas, each with a separate RF chain (59). These additional RF chains lead to a prohibitive cost. Second, they often fail to provide strong security guarantees. On the one hand, fixed-beam directional antennas cannot physically limit signals within an arbitrary area of interest due to their fixed radiation patterns. On the other hand, multi-user beamforming systems (e.g., 802.11ac APs) cannot differentiate intended and malicious clients and strengthen signals for both types of clients. Third, they require significant configuring efforts due to rich multi-path effects indoors (5; 12; 45). Users must try different antenna configurations to identify the one best matching the desired coverage.
1.3 Approach

In this paper, we present a low-cost, physically-secure, and easy-to-configure approach that customizes each AP’s coverage without requiring directional antennas. Given the increasing popularity and easy accessibility of 3D printers, we study the use of 3D-fabricated reflectors produced by 3D digital manufacturing (“3D printing”) to control signal propagation in the space. Specifically, we place a signal reflector around an AP, where the reflector shape is computationally optimized, taking into account the environment (e.g., interior layouts, partitions, AP locations) and the desired signal distribution (i.e., target areas to strengthen or weaken signal strength). The reflector reflects wireless signals to realize a desired coverage. Indeed, anecdotal experiments (67) have demonstrated substantial (29.1% – 57.2%) bandwidth gain by placing a soda can behind a Wi-Fi AP to strengthen signal in one direction. Our work generalizes this idea by presenting a systematic approach to optimizing reflector shapes for enabling a rich set of signal distributions.

Specifically, our system works as follows (Figure 1.1). Users first provide the system with a digitized environment setup (e.g., furniture, floor plan), which can be obtained using full-fledged systems (e.g., Google Tango, Microsoft HoloLens) or other 3D geometry reconstruction techniques (16; 31; 54). Users then specify AP locations, as well as target areas to strengthen or weaken wireless signal strength. With these inputs, the system automatically computes a 3D reflector shape that considers the signal’s interaction with the given environment to form the target wireless coverage.

The shape optimization is an iterative stochastic optimization process that searches for a 3D reflector shape for each AP, so that collectively they achieve the target wireless coverage. Starting from an initial 3D shape and reflector position, our algorithm perturbs the current shape and estimates the resulting signal distribution with the new shape. Based on an objective function that measures the quality of a reflector shape, it then
**Figure 1.1:** Overview. Our system takes the following input: a 3D environment model, the AP location, and target signal coverage. It then iteratively searches for a 3D reflector shape optimized to achieve the target signal distribution. Users simply press the button of a 3D printer to fabricate the reflector, and mount the fabricated reflector around the AP to realize the target signal distribution. We examine the signal distribution through drone-based measurements.

chooses to accept or reject the perturbed shape before moving on to the next iteration.

Evaluating the objective function requires a 3D wireless propagation model that predicts the spatial distribution of received signal strength. Our wireless propagation model takes into account the indoor environment and simulates the radio waves interacting with environment objects. The process stabilizes at a final shape until no further improvement can be made to better match the target.

Finally, we output the shape and placement of the reflector, then the user fabricates the optimized reflector shape and coats it with a thin metal layer (e.g., aluminum foil) to enhance its ability to reflect wireless signals. The fabricated reflector is then mounted around the wireless AP to realize the desired wireless coverage.
1.4 Contributions

Our approach provides four benefits. First, it provides strong physical security by limiting the physical reach of wireless signals, hence creating a virtual wall for wireless signals. Second, it relies on a low-cost ($35), reproducible 3D reflector, which can be easily replaced upon substantial changes in the environment or coverage requirement. Third, it offers an easily-accessible and easy-to-configure solution to non-expert users. Users only need to specify coverage requirements and a coarse environment model, with which our system computes a reflector shape tailored to the built environment. Figure 1.2 illustrates example beam patterns enabled by various reflector shapes. Finally, it is applicable to commodity low-end Wi-Fi APs without directional or multiple antennas.

Table 1.1 compares our solution to its alternatives. Though fixed-beam directional antennas (e.g., microstrip antennas (5)) have relatively low cost (a few dollars), it typically concentrates signals in a single static direction thus has low flexibility. Meanwhile, configurable-beam directional antennas offer multiple beam patterns and dynamic configuration of beam patterns but come with high price tags (e.g., $5000+ for Phocus array (29)). However, both of them present a steep technical barrier to ordinary users, who may not have sufficient domain knowledge to configure antennas based on their environments. On the other hand, multi-user beamforming systems (e.g. 802.11ac APs) collect
<table>
<thead>
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<th>Physical Security</th>
<th>Config. Effort</th>
<th>Hardware Cost</th>
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<td>Fixed-beam DA</td>
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<td>High</td>
<td>Low</td>
<td>Good</td>
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<td>High</td>
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<td>Multi-user beamforming</td>
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<td>Our solution</td>
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Table 1.1

Comparing our solution to directional antennas (DA) or beamforming.

real-time Channel State Information (CSI) to enhance the signal strength for all connected clients without differentiating malicious users, which fail to provide security guarantees. And it usually takes a few hundred bucks. In comparison, we offer a physically-secure, low-cost, and easy-to-configure solution in this paper.

We have made two key technical contributions in this work: First, we design an effective optimization algorithm that optimizes reflector 3D shapes for a target wireless coverage. During this process, we represent a reflector shape as a parametric model (53) in computer graphics to ensure surface smoothness and in turn the feasibility of 3D fabrication. The shape optimization leverages a 3D wireless modeling to evaluate the effectiveness of a candidate shape and improve the shape iteratively. We guide a Simulated Annealing algorithm (36) using local gradient descent to sample the shape space more efficiently. We also extend our optimization to deal with multiple APs and jointly optimize their reflector shapes. Second, we develop an efficient modeling approach that uses 3D ray tracing to simulate radio signal propagation and signal’s interaction with objects in a 3D environment. We consider signal’s reflection, transmission, and diffraction through objects. For APs with multiple antennas, we also take into account the antenna location and orientation to trace radio signals accurately in the 3D space.

We 3D print optimized reflectors, test them with various Wi-Fi APs (including the latest 802.11ac AP) via signal and throughput measurements in two indoor settings. Our findings are as follows:
• Optimized reflectors correctly adjust signal distribution towards the target coverage. Resulting signal strength can decrease by up to 10 dB and increase by 6 dB, leading to throughput differences from -63.3% to 55.1%;

• Optimized reflectors coexist nicely with various Wi-Fi APs including MIMO APs (e.g., TP-Link AP and Netgear R7000). They allow multiple APs to collaboratively serve a region, or to confine each AP’s coverage to enhance security and reduce interference;

• The optimized reflector is relatively easy to place. Its efficacy is not sensitive to slight placement offsets, tolerating up to 10° offset in orientation and 10 cm offset in the distance to the AP.

• Given an environment model, our system computes an optimized reflector shape in 23 minutes on a laptop (2.2 GHz Intel Core i7).

1.5 Outline

The remaining chapters are organized as follows:

In Chapter 2, we review previous research in wireless coverage configuration, directional antennas, and wireless propagation modeling to explain groundwork the thesis builds upon.

In Chapter 3, we focus on shape optimization algorithm. We use NURBS surface to represent the reflector’s shape, simulated annealing combined with gradient descent to search the optimum shape.

In Chapter 4, we describe our shape optimization algorithm. We use NURBS surface to represent the reflector’s shape, simulated annealing combined with gradient descent to search the optimum shape. At last we fabricate the reflector using 3D printer.

In Chapter 5, we introduce the 3D wireless signal propagation model to simulate signal distribution given an 3D indoor layout and position of an AP. We leverage ray tracing
methodology to trace the interaction between every ray and the indoor layout.

In Chapter 6, we first go over the implementation details, including 3D model construction, algorithm implementation, and reflector fabrication. Then we comprehensively evaluate our approach by experimenting several indoor scenarios in two different room layout. We examine the optimized reflectors’ impact on signal distribution and throughput in both single-AP and multi-AP settings. We also test our system’s sensitivity to the reflector placement and size, accuracy of our 3D wireless modeling and running time of the shape optimization.

Finally in Chapter 7, we discuss conclusions of the thesis and outline the limitations and future work.
Chapter 2

Related Work

2.1 Configuring Wireless Coverage

Prior works have optimized AP placement to improve signal reception in certain areas (47). However, moving the AP to enhance one area would result into the decline of signal strength in other areas. Thus, such methods are constrained in its flexibility.

Another method is to use directional APs to confine wireless coverage to a specified region (60). However, this method needs multiple costly directional APs. Other methods either only enhance signal reception (e.g., Wi-Fi range extender) or impose expensive measurement overhead, e.g., the transmit beamforming (44) in 802.11ac APs needs to collect real-time Channel State Information (CSI) to form the optimal beam. Our approach works with a single AP without directional antennas and considers signal’s interaction with the environment to achieve a target coverage.

As for the use of reflectors, recent work (19; 64; 65) has studied reusing walls to reflect radio waves and control signal propagation. This method, however, relies on smart walls made of special materials and requires infrastructure-level changes. Similarly, a latest work (27) examined placing multiple metal plates in the environment to enhance wire-
less performance of a single AP. This approach also requires nontrivial changes in the environment by installing reflectors likely in large sizes. In contrast, our approach uses only a small reflector at the AP, is applicable in any environment, and supports multiple APs. Additionally, (27) optimizes reflector locations, whereas our work optimizes reflector shape. Another prior work (15) studied the feasibility of applying fabricated reflector to control wireless coverage, where the optimized reflector was evaluated using simulations. It uses a simplified shape model, applies standard annealing with 2D wireless modeling, and examines optimized shapes using simulations. We advance this prior work in multiple fronts: a more sophisticated shape model, a more efficient shape optimization and extension to multiple APs, 3D wireless modeling, and extensive indoor experiments with optimized reflectors.

2.2 Directional Antennas

Directional antennas increase signal gain in a chosen direction and thus improve spatial reuse (5; 12; 13; 43; 52; 62; 63). Researchers have studied steerable-beam directional antenna’s link quality outdoors (13). The same directional antenna is also used to study its directionality and impact on node localization and spatial reuse in indoor scenarios (12). However, several existing works show that in indoor settings its directionality greatly decreases due to rich multi-path effects (5; 12; 45). In comparison, we consider the influence of indoor layout when optimizing reflector shape. Besides, high-end directional antennas (e.g., Phocus Array (29)) that offer sophisticated beam control are expensive, while low-cost directional antennas (e.g., microstrip antennas (5), sectorized antennas (63)) only provide limited simple patterns. Our reflector is low-cost and flexible in radiation patterns.

Directional antennas often rely on multi-antenna beamforming, which electronically ad-
justs an array of omni-antennas to form narrow beams and maximize the signal strength for one or multiple users (44; 59). Despite its superior performance, it has three main limitations. First, it cannot provide physical security, as it only enhances client’s signal reception and cannot take into account client’s location information (i.e., whether the client is inside the authorized location or not). As a result, it can end up forming a beam towards an attacker outside the authorized area. Second, it is more costly than our solution as it requires multiple antennas, each with a separate RF chain. Finally, it imposes expensive measurement overhead by collecting real-time Channel State Information (CSI).

2.3 Wireless Propagation Modeling

Active research has studied the modeling of wireless propagation (6; 30; 33; 50). A recent study models the RF propagation as EM waves using the Helmholtz equation (1). This method creates a more nuanced signal map and yet entails a high computational complexity. By contrast, Ray tracing method is known for its efficiency and accuracy (20; 32; 38; 47; 58; 69). Ray tracing simulates the wireless signal propagation as a finite number of isotropic rays emitted from a transmitting antenna. Each ray transmits with the same amount energy from the antenna and the energy attenuates as travel distance increases and encounter walls or floors.

There are two main methods among ray-tracing methods: Image method (32) and Shooting-and-Bouncing Ray (SBR) launching algorithm (20; 38; 58) are two main ray-tracing methods. Image method determines a ray trajectory between a transmitter and a receiver by placing artificial sources that model reflections from the flat surfaces of objects. One problem of image method is in 3D indoor model considering multiple reflections and transmissions, its computational cost will grow exponentially as the number of planes
Image method is best suited for simplified, two-dimensional scenario (20). Meanwhile, in SBR algorithm rays are launched from the transmitter and are traced to see if they hit any object until they reach a receiver. The computational efforts is linear with the number of planes, thus is preferable in complicated, three-dimensional environment with hundreds or thousands of planes and multiple reflections. We adopt SBR launching algorithm in our model. However, our approach does not require specific propagation models and can be integrated with other advanced models.

2.4 Automated Wireless Measurements

Collecting detailed wireless measurements commonly requires intensive human efforts. Prior works have proposed the use of a Roomba robot vacuum with a Wi-Fi receiver to automate signal measurements (24; 25; 35). Red tapes laid our with blue periodic marks indicating spot locations are used to navigate the Roomba to move precisely. However, Roomba is a vacuum cleaning robot on the ground, which is not suitable for our 3D wireless signal measurement. More human-friendly way is to control the drone by making body gestures (14; 26). The disadvantage of this method in our scenario is that the drone itself couldn’t know its measurement locations. It is also difficult to control the drone to precisely stay at one location for a period of time indoor. Drone’s fast moving propellers cause unpredictable airflow in complicated indoor environment, which makes itself drift. In our paper, we adopt the drone-based measurements method. To address aforementioned challenges, we place periodic marks on the ground and leverage drone’s bottom camera to locate and navigate the flight.
2.5 Caustic Design in Computer Graphics.

Our approach echoes the principle of the caustic design in computer graphics, which creates an object between a light source and a planar screen to refract or reflect the light rays and form a desired image on the screen (21; 48; 49; 57; 71; 74). One of the earliest work is to get a target reflectance distribution of a surface by modifying small-scale geometric features on the surface (71). Another work optimized a transmissive or reflective surface that refracts lights from a light source to form an a priori defined caustic image (21). They optimized the surface by using simultaneous perturbation stochastic approximation to minimize the mean squared error between the target caustic image and the caustic image generated by the current surface. However, they evaluated their approach in simulation without any fabrication. Another method uses nonnegative image decomposition based on a set of estimated anisotropic Gaussian kernels, to construct an array of continuous surface patches that focuses lights onto those kernels (49). And it is also the first work that actually fabricate the refractors with a engraving machine. Another interesting application of caustic design is optical hidden image decoding (48), where you can only see meaningful target images with some optimized lens.

In a similar sense, we create an object (the reflector) that steers radio waves to form a signal "caustic pattern" (signal map). Caustic designs rely on advanced 3D optimization to transform an unperturbed light pattern to a desired light pattern. They also require high precision in light propagation. However, in our context, the level of variance for radio wave propagation is high, thus a simpler solver using Monte Carlo method suffices.
Chapter 3

Reector Shape Optimization

The core goal is to fabricate a reector with optimized shape to achieve desired signal map coverage. Thus, given a 3D indoor floor map, the AP’s position, desired signal map coverage and an initial reector, we design a shape optimization algorithm to calculate the best reector’s shape. We first present parameterizing the 3D geometry of a reector, followed by our shape optimization procedure, as well as its extension to deal with multiple APs.

3.1 Representing the Reector Shape

To represent a 3D surface, we seek a shape parameterization that can express a large space of feasible shapes and yet entail a low control degrees of freedom for the sake of computational performance. A naive solution is to represent a shape as a triangle mesh and optimize the positions of mesh vertices. However, this approach has a large number of optimization variables (i.e., the positions of mesh vertices). It results into an optimization problem in a high dimensional space, which is rather computationally expensive. Furthermore, the resulting shape might not be well-formed and thus cannot
be fabricated in practice.

We overcome this challenge by leveraging the Non-uniform rational B-spline (NURBS) surface (53), a shape parameterization commonly used in computer graphics and engineering design (17). The NURBS surface offers appealing properties: 1) it is flexible, supporting a large variety of shapes including standard analytical shapes such as spheres and free-form shapes; 2) it guarantees a smooth surface, facilitating the fabrication; and 3) it enables fine-grained control with low complexity using a small number of control points. and 4) it is invariant under affine transformation, thus rotation and translation could be applied to the surface by directly applying to the control points.

The NURBS surface is defined by NURBS curves. A NURBS curve consists of a set of weighted control points, a knot vector and its order. We aim to fit control points on the curve, which then determine the curve shape. The knot vector is a list of ascending numbers, defining where and how control points affect the NURBS curve. By manipulating the knot vector, we can decide whether the curve passes through or passes by certain control points. The size of the knot vector is equal to the number of control points plus the order. The order defines the number of nearby control points that influence any given point on the curve.

A NURBS surface is calculated as the tensor product of two NURBS curves. Thus, it has two parametric directions ($u$ and $v$) and two corresponding orders and knot vectors. For our purposes, we predefine its knot vectors and orders and then manipulate its shape by changing positions of the control points. A NURBS surface $\Omega(u, v)$ is constructed as:

$$\Omega(u, v) = \sum_{i=1}^{l} \sum_{j=1}^{w} R_{i,j}(u, v)P_{i,j},$$

with

$$R_{i,j}(u, v) = \frac{N_{i,n}(u)N_{j,m}(v)w_{i,j}}{\sum_{p=1}^{l} \sum_{q=1}^{w} N_{p,n}(u)N_{q,m}(v)w_{p,q}}$$

(3.2)
as rational basis functions, where we have $l \times w$ control points $P_{i,j}$, and $w_{i,j}$ is the corresponding weight. $N_{i,n}(u)$ is the $i^{th}$ B-spline basis function of degree $n$ (18). In our model, a shape $\Omega$ is defined by $l \times w$ control points $P_{i,j}$.

### 3.2 Optimizing the Reflector Shape

To search for the reflector shape optimized for a target coverage, we start with a flat plane as the reflector shape $\Omega$ and then perturb $\Omega$ over iterations. In each iteration, we evaluate the effectiveness of a candidate shape $\Omega$ by the objective function $F(\Omega)$, where $F(\Omega)$ measures the difference between the desired coverage and the coverage $C_{\Omega}$ resulting from reflector shape $\Omega$. We estimate $C_{\Omega}$ by running the 3D wireless modeling described in Section 4. Specifically, we divide the environment into small cells in uniform size (1 m $\times$ 1 m in our implementation). We apply the 3D wireless propagation modeling to predict signal strength at each cell’s center. Assuming $M_+$ and $M_-$ denote the areas where users aim to strengthen and weaken signals respectively, we compute $F(\Omega)$ as:

$$F(\Omega) = \sum_{i \in M_+ \cup M_-} ||C_{\text{Target}}(i) - C_{\Omega}(i)||^2,$$

(3.3)

where $C_{\Omega}(i)$ is the signal strength in dBm at cell $i$ after placing reflector shape $\Omega$, and $C_{\text{Target}}(i)$ is the target signal strength of cell $i$. To derive $C_{\text{Target}}(i)$, we first compute signal $C(i)$, which is the estimated signal strength at cell $i$ when no reflector is placed. We then add/subtract $\delta$, which is the expected signal enhancement/reduction at cell $i$. To determine $\delta$, we tested different materials on their performance of signal enhancement and attenuation at distances from 1 to 3 meters. Results (Figure 5.9) show that the signal
Figure 3.1: (a) shows the objective function $F(\Omega)$ as we perturb two control points of the NURBS surface. (b) illustrates our search method. In the $(k-1)$-th iteration ($\Omega_{k-1}$), we apply gradient descent to seek the local optimum $\Omega_k'$ and choose $\Omega_k'$ as the next candidate.

Change is at most 15 dB. Thus we set $\delta$ to 15 dB and write $C_{\text{Target}}(i)$ as:

$$
C_{\text{Target}}(i) = \begin{cases} 
C(i) + \delta & \text{if } i \in M_+ \\
C(i) - \delta & \text{if } i \in M_- 
\end{cases}.
$$

(3.4)

Here we use a cell-dependent target value $C_{\text{Target}}(i)$, rather than a uniform signal upper and lower bound, because $C_{\text{Target}}(i)$ defines an equal range ($\delta$) above or below $C(i)$. As a result, a given amount of signal enhancement or reduction leads to the same amount of change in $F(\cdot)$, regardless of the cell location. This, however, is no longer guaranteed if a uniform bound is used, because of the quadratic nature of $F(\cdot)$. Thus, $C_{\text{Target}}(i)$ ensures the optimization process is unbiased across cells. Finally, the optimization process searches for $\Omega^*$: $\Omega^* = \arg\min_{\Omega} F(\Omega)$, where $\Omega^*$ is the 3D reflector shape that leads to signal distribution best matching the target.

While the optimization problem appears standard, the search space is daunting and many local optima exist (Figure 3.1(a)). Simple local search methods such as hill climbing can easily be stuck at local optima. We need efficient algorithm to identify the global optimal. To achieve this goal, we consider simulated annealing (SA) (36), which allows the iterations to opportunistically escape from the current local search area even if the escape
Algorithm 1 Shape Optimization

1: initialize $\Omega_k$, $k = 0$, $T = T_{max}$
2: while $T > T_{min}$ do
3:     $k \leftarrow k + 1$
4:     $F(\Omega_{k-1}) \leftarrow$ Eq.(3.3)
5:     $\Omega_k \leftarrow$ perturb($\Omega_{k-1}$)
6:     while do
7:         $\nabla F(\Omega_k) \leftarrow$ getGradient($F(\Omega_k)$)
8:         $\lambda \leftarrow$ getStepSize()
9:         if $F(\Omega_k - \lambda\nabla F(\Omega_k)) + \epsilon < F(\Omega_k)$ then
10:             $\Omega_k \leftarrow \Omega_k - \lambda\nabla F(\Omega_k)$
11:         else
12:             break
13:     end while
14:     $F(\Omega_k) \leftarrow$ Eq.(3.3)
15:     $p \leftarrow e^{-\frac{F(\Omega_{k-1}) - F(\Omega_k)}{T}}$
16:     if $F(\Omega_{k-1}) \geq F(\Omega_k)$ or rand[0,1] $\leq p$ then
17:         $\Omega^* \leftarrow \Omega_k$
18:     end if
19:     $T \leftarrow T \cdot r$
20: end while
21: return $\Omega^*$

leads to an increase in the objective function. The escape likelihood $p$ is determined by two parameters in the algorithm: current temperature $T$ and the increase in the objective function. SA keeps examining candidate shapes until $T$ reaches the minimal temperature (0). When a candidate shape $\Omega$ is examined, the current temperature is cooled at a rate $r$. SA accepts $\Omega$ if $F(\Omega)$ is lower than the previous candidate. Otherwise, it accepts $\Omega$ with a probability $p$. $p$ is adapted over iterations. In the beginning when $T$ is higher, $p$ is also higher so SA tends to explore other areas in the shape space. As $T$ decreases to 0, $p$ approaches 0 so that it gradually settles at an optimum.

However, SA can require a fairly large number of iterations as it randomly samples the search space. To achieve better results, we propose to guide SA’s iterations using gradient descent. The key idea is to consider characteristics of a local search area for determining the next candidate. Specifically, in each iteration of SA, instead of randomly generating a shape as the candidate, we apply gradient descent to seek the local minimum as the next candidate. Take the $k$th iteration as an example, we first generate a random shape $\Omega_k$,
then we calculate the shape gradient $\nabla F(\Omega_k)$ of objective function $F(\Omega_k)$ at $\Omega_k$:

$$\nabla F(\Omega_k) = \lim_{||d\Omega_k|| \to 0} \frac{F(\Omega_k + d\Omega_k) - F(\Omega_k)}{d\Omega_k},$$

(3.5)

where $d\Omega_k$ is obtained by slightly changing the control points of $\Omega_k$. Then we apply backtracking line search to find an appropriate step size $\lambda$. Finally we take $\Omega_k - \lambda \nabla F(\Omega_k)$ as $\Omega_k$ and repeat Eq. (3.5) until we find a local optimum $\Omega'_k$. We take $\Omega'_k$ as the candidate instead of $\Omega_k$ to go over the accept/reject procedure. This method directly iterates from one local minimum to another (Figure 3.1(b)), and thus is more efficient to approach the global optimum than SA’s random sampling (41).

Each iteration in our search can be time-consuming, because deriving $\nabla F(\Omega_k)$ requires altering the positions of $\Omega_k$’s control points one by one. The running time of each iteration is linear with the number of $\Omega_k$’s control points. Thus, we speed up each iteration as follows. First, we carefully balance the optimization efficiency and shape precision by choosing $3 \times 5$ control points. Fewer control points fail to support the variety of shapes, while more control points result in twisted shapes and even worse result due to the enlarged search space. Moreover, to speed up the gradient computation, we leverage the simultaneous perturbation stochastic approximation (SPSA) algorithm (11; 61), which perturbs all parameters (i.e., control points) simultaneously with a random perturbation vector $\Delta$ to estimate the gradient of each parameter. Thus, it approximates the gradient computation using only two calculations of the objective function, regardless of the parameter dimension (i.e., the number of control points in our problem). Additionally, we run these iterations as parallel threads to further shorten the process. As a result, an iteration take 1.71 seconds on average on a MacBook Pro (2.2 GHz Intel Core i7).
3.3 Extending to Multiple APs

We now extend the above shape optimization to handle multiple APs. We classify APs into two types: 1) **Collaborative APs**: APs that are deployed by the same entity, e.g., a user or an enterprise deploying multiple APs in a home or workplace. These APs collaboratively serve a region to provide wireless coverage and user’s device automatically connects to the AP with the strongest signal; 2) **Non-Collaborative APs**: APs that are deployed by different entities. Each AP serves users in its own pre-defined coverage region, without the knowledge nor any control of other APs.

For collaborative APs, we jointly optimize their reflector shapes so that the resulting signal coverage best matches the target. Here the signal coverage map is defined based on the strongest signal received at a location from all collaborative APs. Thus, let $\Omega = \{\Omega_1, ..., \Omega_M\}$ denote a set of candidate reflector shapes for $M$ collaborative APs, where $\Omega_j$ is the reflector shape for AP $j$. Then its objective function $F(\Omega)$ is similar to Eq.(3.3):

$$F(\Omega) = \sum_{i \in M_{+}\cup M_{-}} ||C_{\text{Target}}(i) - C_\Omega(i)||^2,$$

(3.6)

For non-collaborative APs, each AP has its own pre-defined coverage region without the knowledge of other APs, thus each AP’s reflector shape is optimized separately following the Algorithm. For non-collaborative APs operating on the same channel, they can interfere with one another if their coverage regions are nearby. The impact of interference can be minimized if the information (e.g., location, reflector shape) of other interfering APs is available to the shape optimization algorithm. We can estimate the interference at each cell and consider signal-to-interference ratio (SINR) as the target (Eq. (3.3)) for shape optimization. We leave it for future work.
Chapter 4

Efficient 3D Wireless Modeling

Another essential part of our method is an efficient modeling that simulates wireless signal propagation in a given environment for evaluating the efficacy of a candidate reflector shape. Most existing models either fall far short in modeling accuracy (37; 50), or require expensive measurement or computation overhead. In our context, we desire a better tradeoff between accuracy and efficiency, since the propagation model is run repeatedly to evaluate the efficacy of a reflector shape during the shape optimization process. To achieve a better tradeoff, we choose 3D ray tracing for its best accuracy (32; 47; 69) and design schemes to speed up its computation. In particular, we choose the Shooting-and-Bouncing Ray (SBR) launching algorithm (20; 38; 58), which launches a number of rays from the transmitter and traces all their possible paths to reach a receiver. Specifically, our 3D propagation modeling takes two inputs: 1) a 3D environmental model (e.g., a 3D floor plan), and 2) the AP location and antenna configuration (e.g., the number of antennas, antenna orientation and placement). Next we describe the key steps of our modeling in detail.
Figure 4.1: Geodesic sphere for uniform ray launching, where a ray is emitted from the sphere center to each geodesic vertex on the sphere. The sphere is generated by tessellating a regular icosahedron (a). (b) and (c) show the resulting spheres after tessellating each triangle surface in (a) into 4 and 256 triangles, respectively.

4.1 Ray Launching

In our 3D wireless propagation model, the radio waves from a transmitter are modeled as many uniformed rays shooting from the location of the antenna. It is desirable to model each launching ray uniformly and predictably distributes around the transmitter, which means equal angles between a ray and its neighbors. Past work demonstrates ray launching from the vertices of regular polyhedrons is the only way to fulfill this criteria (66).

Our method is to use geodesic sphere ray launching, which is formed by tessellating the faces of a regular polyhedron and extrapolating the intersection points of the surface of a sphere (34). The geodesic vertices provide equivalent angular separation around the entire sphere (58), thus we can model the ray launching from the center of the sphere to every geodesic vertex on the sphere to guarantee uniform ray launching. We consider tessellating an icosahedron in our model.

An regular icosahedron has 20 triangular faces and 12 vertices. To achieve higher resolution, we can tessellate each triangular face of the icosahedron into \(N\) equal segments, where \(N\) is called tessellation frequency (70), shown as Figure 4.1. Then the number of total geodesic faces is \(20N^2\) and number of total geodesic vertices, which is also the ray
number, is $10N^2 + 2$. There are some discrepancies in angular separation among launched rays, however it can be mitigated by using higher tessellation frequency (58) and adopting average angular separation. By equating the $20N^2$ geodesic faces within a $4\pi$ steradians unit sphere, we can find the approximately average radial angular separation as (20):

$$\alpha = \frac{1}{N} \sqrt{\frac{4\pi}{5\sqrt{3}}} = \frac{1.205}{N} \text{ radians},$$  \hspace{1cm} (4.1)

### 4.2 Ray Tracing

We track each ray’s interaction with environmental objects. Given the wavelength of Wi-Fi signals, we consider three types of interactions (Figure 4.2(a)): transmissions (rays penetrate the objects), reflections (a ray is bounced over a smooth surface), and diffractions (a ray hitting an object edge is diffracted as a set of rays in a cone shape, Figure 4.2(b)). To model diffraction, we leverage the Uniform Theory of Diffraction (UTD) used by the fast-wave acoustics simulation in computer graphics (68). It has also been applied in modeling RF propagation in buildings (51). Similar to (28; 32), we do not consider wave phase as we average signal strengths in each $1 \text{ m} \times 1 \text{ m}$ cell when evaluating coverage.

We do not model other wave phenomena like scattering since they have negligible impact on the resulting signal map (32). Though wireless radiation near field behaves differently from far field, we ignore the near field effects because the border between near field with far field is the Fraunhofer distance $2D^2/\lambda$ from the antenna (9), where $D$ is the largest physical linear dimension of the antenna and $\lambda$ is the wavelength. In our scenario, the Fraunhofer distance only counts for tens of centimeters while our measurements lie at least meters from the antenna.

While offering higher accuracy, ray tracing incurs heavy computation, mainly because of calculating intersections of a large number of rays and triangle meshes. In our implemen-
Figure 4.2: Ray tracing.

tation, the indoor model has 107 triangle meshes and the ray tracing launched 1926 rays, producing \( \approx 10^K \) rays after multiple reflections and transmissions. To speed up the ray tracing process, we index the triangle meshes with a Kd-Tree (10). We construct a Kd-Tree of the bounding boxes containing these triangle meshes. For each ray, we first search the tree to identify the bounding boxes that the ray intersects. Only for the triangle meshes in those bounding boxes, we examine the ray-triangle intersection, which avoids many unnecessary intersection tests. For each ray-box and ray-triangle intersection test, we apply prior algorithms (23; 42) to improve the efficiency.

4.3 Path Loss Model

Each type of ray interaction contributes to additional energy loss of a ray, in addition to its signal degradation over distance. To integrate all these contributors, we choose a partition model (7; 32) to calculate each ray’s signal power at a receiver location. The model consists of four parts: 1) the signal degradation over distance, represented by the pathloss exponent \( \alpha \); 2) the reflection attenuation, which is the product of the reflection coefficient \( \beta \) and the number of reflections; 3) the transmission attenuation, which is the product of the transmission coefficient \( \gamma \) and the number of times that a ray penetrates obstacles; and 4) the diffraction attenuation, which is the product of the diffraction co-
efficient $\lambda$ and the number of diffractions. We do not consider multiple diffractions and reflection-diffraction (58).

Formally, let $P_i^j$ denote the power in dBm contributed by the $i^{th}$ ray of $j^{th}$ AP after traveling a distance of $d_i$ to reach a receiver, we can calculate $P_i^j$ as:

$$P_i^j = P_0^j - 10\alpha \log_{10}(d_i/d_0) - \beta N_{i,\text{ref}} - \gamma N_{i,\text{trans}} - \lambda N_{i,\text{diff}} - \beta' N'_{i,\text{ref}} - \gamma' N'_{i,\text{trans}}$$

(4.2)

where $P_0^j$ (in dBm) is the reference power of $j^{th}$ AP at distance $d_0$, pathloss exponent $\alpha$ captures how quickly the signal degrades over distance, $N_{i,\text{ref}}, N_{i,\text{trans}}, N_{i,\text{diff}}$ are the number of reflections, transmissions, and diffractions that ray $i$ experiences, respectively. Since the reflector surface is designed to be highly reflective, we consider different transmission and reflection coefficients ($\beta', \gamma'$) for the reflector. $N'_{i,\text{ref}}$ and $N'_{i,\text{trans}}$ are the number of times ray $i$ penetrates and is reflected by the reflector, respectively.

### 4.4 Ray Reception

To calculate the received signal strength at a receiver location, we need to define a reception zone first. We consider the reception zone as a sphere with radius of $\theta d / \sqrt{3}$ centered at the receiver (56), where $\theta$ is the average radial angular separation between adjacent rays launched from the transmitter, and $d$ is the length of a ray’s propagation path to the receiver. The radius of the reception sphere considers the fact that rays are spread out as they propagate. Figure 4.2 shows the reception sphere for each ray, where ray2 travels the longest distance to reach receiver and thus has the largest reception sphere. The radius of the reception sphere is configured as $\theta d / \sqrt{3}$ because the linear distance between rays is nearly $2\theta d / \sqrt{3}$.

We calculate the received power $P_j^i$ (in dBm) from $j^{th}$ AP as the summation of the power
of all rays within the reception sphere $Z$ at the receiver location \(^{(69)}\). After acquiring each ray’s path loss, we convert the path loss (dBm) of each ray to power (watts), sum the power of each ray within the reception zone $Z$ of this receiver, then convert the sum to dBm to get the aggregate path loss value as followings:

$$P^j = 10\log_{10} \sum_{i \in Z} 10^{P^j_i/10},$$  \hspace{1cm} (4.3)

where $P^j$ (in dBm) is the received power from AP $j$ and $P^j_i$ (in dBm) is the power contributed by ray $i$ from AP $j$ calculated by Eq. (4.2).

Finally, we need to calibrate the reference parameters $P^j_0, \alpha, \beta, \gamma, \lambda, \beta', \gamma'$ in Eq. (4.2) to apply our path loss model. With some measurements only at a few sampled locations, we apply simulated annealing to find the best-fit parameters values that minimizes the simulation errors. Notice that in our ray tracing model, the reflection coefficient and transmission coefficient of the reflector are considered separately since the reflector is supposed to have better reflectivity. These parameters can then be reused at all locations of an environment.
Chapter 5

Evaluation

We evaluate our approach by testing optimized reflectors in two indoor scenes. We seek to understand its capability in affecting wireless signal distribution and throughput, implications on enhancing security and reducing interference, its sensitivity to reflector placement and size, and other performance microbenmarks.

5.1 Implementation

In order to simulate 3D wireless propagation indoor, we should have accurate site-specific indoor information. We use Blender (22), an open-source 3D computer graphics software, to build a 3D model of indoor environment(Figure 5.1(a)). We select this tool because it can export .obj file, which contains positions of vertices and faces. Only large-scale features indoor are considered, such as walls, doors, tables, refrigerators and so on. Blender can create surfaces that mimic the shapes of real-world objects e.g., tables, sofas, and walls. Among the three types of modeling offered by Blender, namely mesh, curve, and meta modeling, the mesh modeling was most suited to our scenario.

We implement the wireless signal modeling (i.e., ray launching, ray tracing, ray recep-
Figure 5.1: (a). 3D indoor model built by Blender. (b). Top view and side view of ray tracing visualization by OpenGL. 42 rays are launched in this example, and the maximum times of transmission and reflection is 4 and 3.

We parse .obj file of 3D indoor model and visualize how each ray interacts with environment as in Figure 5.1(b) to validate the correctness of ray tracing process using JOGL (3). The JOGL provides full access to the APIs in the OpenGL to applications written in Java. For shape optimization, we use jMonkeyEngine SDK (2) to construct a NURBS surface via defining control points, knot vectors and other parameters. To reduce the dimensions of search space, we use 3 by 5 control points, uniform knot vectors, set both orders to 3, and all weights as 1. We optimize the shape by only perturbing the positions of control points. In future work, however, the weights and knot vectors can be also optimized to generate more sophisticated shapes with slightly higher computational cost.

After we obtain the optimized shape $\Omega^*$, the last step is to realize it as a physical reflector. We output all the mesh points of $\Omega^*$ in an .obj file, add thickness to the surface and export it to a .stl file for a 3D printer (MakerBot) to print it. Its build volume is 25.2 cm $\times$ 20 cm $\times$ 15.0 cm. Overall fabricating a 20 cm $\times$ 20 cm reflector costs no more than $35 (one large spool of MakerBot PLA Filamen). We add a thin layer of metal to the plastic reflector surface because metals have exceedingly high conductivities and thus are effective reflectors and attenuators of radio waves (46). In Sec 5.5, we experiment
Figure 5.2: Two experiment scenes, where scene 1 is a typical workspace scenario, while scene 2 has a spacious lobby room surrounded by three rooms, resembling a private home scenario. (a). We automate the Wi-Fi signal measurements using a drone (AR Drone 2.0), where we place paper marks on the floor for the drone to navigate across measurement locations autonomously.

with different metals (copper, silver, and aluminum) and choose aluminum given its good performance and lower cost.

5.2 Experimental Setup

We experiment two indoor scenarios with different room layouts: (a) a 19 m × 13 m indoor area with a narrow (7.5-m long) hallway connecting a research lab and two offices (Figure 5.2(a)); (b) a 16 m × 12 m area where a spacious lobby (5.8 m × 5.1 m) is surrounded by three rooms (Figure 5.2(b)). Figure 5.3(a) and Figure 5.5(a) show their floor maps, respectively. Although rooms are furnished in both scenes, the 3D environment models used in our shape optimization contain only walls and doors (we will evaluate the impact of including furniture in environment models in later chapters). Experiments are conducted during working hours with moving users around (walking, working at their desks, or standing and talking to others). For the simplicity and feasibility of the user input, we assume the same material for objects in the environment.
We use Netgear R7000 (IEEE 802.11ac) as default APs. R7000 has three antennas and operates on both 2.4 GHz and 5 GHz frequency. We configure it to transmit at 10 mW and collect RSS values at 2.4 GHz band. We also test two other popular APs: Linksys WRT54GL (IEEE 802.11g) and TP-Link WR841N (IEEE 802.11n), both operating on 2.4 GHz frequency and equipped with two external antennas. To minimize interference from external APs, we analyze channel usage status using a mobile app (Wi-Fi Analyzer) and set the AP to operate on the least congested channel (channel 9 in our environment).

Although our approach does not require exhaustive site survey measurements to compute reflector shapes, such measurements are necessary for us to evaluate the impact of optimized reflectors on signal distribution. To gather signal measurements, we divide each area into 1 m × 1 m cells and average received signal strength (RSS) values within each cell. We also sample a few locations (blue circles in Figure 5.3(a) and Figure 5.5(a)) to measure the throughput.

To automate RSS measurements in the 3D space, we apply a drone-based method in (73). We program an AR Drone 2.0 to collect RSS at specified locations. We reuse drone’s built-in Wi-Fi radio to receive beacons from our AP and record RSS values. We also leverage drone’s bottom-facing camera for autonomous navigation, guided by paper marks (1-m interval) on the floor (Figure 5.2(a)). Communication with the drone’s controller is done via socket connection and the drone’s command line interface via telnet. During the measurement, the controller sends commands to the drone, thus the RSS should be sufficiently high for stable communication. To decide the measurement duration per location, we let the drone hover over a location, measure for 1 minute and 10 seconds respectively, and compare the mean and standard deviation of RSS. Results reveal that 10 seconds are sufficient for collecting stable RSS statistics.
Figure 5.3: Efficacy of an optimized reflector for achieving a target wireless coverage (a), where areas users aim to strengthen the signal are marked by green ticks and areas to weaken the signal are marked by red crosses. (b) and (c) show a reflector in a simple concave shape and a reflector in optimized shape, while (d), and (e) show their resulting signal changes in dB. The optimized reflector shape leads to a signal distribution better matching the target.

5.3 Efficacy of Optimized Reflector

5.3.1 One-AP Settings

We start by examining the overall efficacy of the optimized reflector in a single-AP setting. We consider a target coverage in Figure 5.3(a), where we mark areas with received signals to be strengthened by ticks and areas with signals to be weakened by crosses. We run our shape optimization algorithm to derive the optimized reflector shape, fabricate the reflector (20 cm × 20 cm in size), and place it around AP’s antennas. Figure 5.3(c) shows the optimized 3D shape, its estimated radiation pattern, and its placement. The radiation pattern is generated by simulating signal change at one meter away. For this target coverage, an antenna is behind the reflector and the others are in front of the reflector. We measure changes in the resulting RSS and throughput.
### Impact on Signal Distribution

We collect the signal maps before and after placing the reflector around the AP. We also compare the results to that of a naive reflector shape (the concave shape used in anecdote experiments, Figure 5.3(b)). Figure 5.3(d) and (e) show the RSS change (in dB), where positive numbers indicate signal enhancements and negative numbers indicate signal declines. We observe that the optimized reflector correctly adjusts signals in all target areas, weakening signals in the hallway and room2 by 10 dB while strengthening signals in other target areas by 6 dB. It achieves the goal by blocking an antenna that emits signals to the hallway and room2 while reflecting the signals of the other two antenna towards room1. The naive reflector, however, generates a simple radiation pattern that uniformly weakens signals in all areas in the back of the reflector, and thus fails to meet requirements of all target areas. The result demonstrates the necessity and efficacy of our optimization, which considers the indoor layout to customize the reflector shape and enables more flexible control.

A side effect of the optimized reflector is that in order to weaken signals in the hallway and room2, it also slightly weakens the RSS in the right bottom of the lab. It is a sacrifice made by the shape optimization to reach an overall signal distribution better matching the target. As we further analyze signal change at individual cells, 83.1% of cells have their signals correctly strengthened or weakened, demonstrating the overall efficacy of the optimized reflector.
Impact on Throughput. We further examine how signal-level changes translate into throughput differences at clients. We sample a few locations (marked as blue circles in Figure 5.3(a)) and measure the throughput at those locations before and after placing the reflector. In particular, we associate two laptops (MacBook Pro) with our AP. We fix the location of a laptop, while a user holds the other laptop walking around within each location to measure the throughput. We instrument one laptop to transmit 500-MB data to the other using the iperf utility and collect throughput statistics. We repeat the experiment for 10 rounds.

Figure 5.4 shows the percentage of throughput change under different APs with optimized reflectors. We also include error bars covering 90% confidence intervals. Overall throughput increases/decreases by up to 22.1%/36.7% in target areas. The throughput improvement at location 8 is small because its RSS is low, requiring a larger signal enhancement to switch to higher data rates. The throughput at location 9 slightly decreases because its RSS is slightly weakened by the reflector (Figure 5.3(e)). Most other locations in the lab experience improved throughput. Overall, the optimized reflector correctly adjusts throughput for 11 out of 12 locations. The result also shows that our reflectors can coexist nicely with MIMO APs (i.e., TP-Link AP and Netgear R7000).

5.3.2 Multi-AP Settings

We now move on to scenarios with multiple APs.

Collaborative APs. To evaluate the efficacy of jointly optimized reflectors, we deploy two APs in scene 2 and jointly optimize their reflector shapes for a target coverage in Figure 5.5(a). We measure the signal map before and after placing reflectors, where the RSS at a location is the signal from the stronger AP. We plot the signal change in Figure 5.5(b). The two optimized reflectors successfully reduce signal strength in lobby by up to 10 dB and increase signals up to 6dB in room 3, 4 and 5 (The numbers are slightly different
Figure 5.5: Efficacy of optimized reflectors of two collaborative APs to achieve a target wireless coverage. In (a), areas where users aim to strengthen or weaken signals are marked by green ticks and red crosses, respectively. (b) shows the map of resulting signal change in dB. (c) plots the throughput improvement at sampled locations (blue circles in (a)).

from that in Figure 5.9 since the result here is measured at further distances and also affected by the environment.). Overall, 91% of cells have their signals correctly strengthened/weakened. To further examine the impact on resulting bandwidth, we sample 9 locations (blue circles in Figure 5.5(a)) and plot in Figure 5.5(c) the throughput change brought by optimized reflectors. For 7 out of 9 locations, the throughput changes from -63.3% to 55.1%. Location 13 and 18 experience little change because of their minor signal changes (Figure 5.5(b)). Overall the signal and throughput changes are notable for the majority of locations, demonstrating the efficacy of our joint optimization.

Non-Collaborative APs. For non-collaborative APs, we aim to confine each AP’s coverage. We examine the implications on security/privacy and interference reduction with optimized reflectors.
1) Implications on Security/Privacy: We set up two Netgear R7000 APs in scene 1 and mark each AP’s coverage region in Figure 5.6(a). We then fabricate reflectors for these APs to confine their coverage. We measure packet loss rates at sampled locations (marked as blue circles) before and after placing reflectors. We associate two laptops (MacBook Pro) with the same AP and instrument a laptop to transmit packets to the other using the iperf utility. Similarly to (60), we desire packet loss rates above 30% for locations outside an AP’s coverage region, as many TCP and UDP based applications (8; 55) require a packet loss rate below 25%.

Figure 5.6(b) plots packet loss rates when a receiver outside an AP’s region attempts to connect to this AP. Before placing any reflector, all locations have access to both APs. After placing optimized reflectors, we find that room2 (location 1 and 2) is unable to
access the network of AP1 (50 - 60% packet loss rates), and locations at the lab (location 6, 7 and 8) can not access AP2. This demonstrates that optimized reflectors help confine Wi-Fi signal strength in the desired region. We also observe that for some locations outside an AP’s region, packet loss rate does not change much after placing the reflector, e.g., the packet loss rate of AP2 at location 9 is nearly 0% with or without the reflector. It is because location 9 is relatively close to AP2 and receives a strong signal from AP2 even with the reflector. The same holds for location 3, 4, and 5. To address this limitation, we plan in future work to include transmit power as another parameter in our model to control coverage more precisely.

2) Reducing Interference: To quantify the benefit on interference reduction, we examine Signal to Interference Noise Ratio (SINR) at locations in each AP’s coverage region. We reuse the setting in Figure 5.6(a) and compute the SINR at all locations. Figure 5.6(c) shows that reflectors boost the SINR for most locations by up to 13 dB. The SINR at location 9 barely changes because while AP2’s reflector weakens the interference, AP1’s reflector also weakens the signal at this location, resulting into little change in its SINR.

5.4 Reflector Placement and Size

In addition to the reflector shape, the reflector placement and size can also affect reflector’s efficacy. Next we examine system’s sensitivity to these factors. In following experiments, we use the optimized reflector in Figure 5.3(c) as an example.

Placement Offset. We first study the impact of orientation offset, which can occur during manual placement. In the experiment, the reflector (20 cm × 20 cm) faces room1 and room2 to enhance signals, which corresponds to the 0° orientation offset. We rotate the reflector from −30° to 30° in a counterclockwise manner with 5° interval. We then plot the average signal enhancement of interested locations in room1 and room2 in
Figure 5.7(a). During the experiment, we observe some large signal variation at certain locations (location 10) when the orientation offset is within $10^\circ$, but the variation is only within 0.51 dB for room1 and 0.83 dB for room2, indicating that the reflector can tolerate small orientation offset. Orientation offset larger than $10^\circ$ results in slow decrease in signal enhancement.

We then examine how the distance between the reflector and AP affects the performance. We fix the reflector’s orientation, vary its distance from 0 cm to 25 cm with 5-cm interval, and plot the average signal enhancement at room1 and room2 in Figure 5.7(b). We observe that offsets within 10 cm have negligible impact. Once the distance is above 10 cm, the signal enhancement starts to decrease. It is because as signals travel, they are further spread out with attenuated strength. Thus, a reflector further away from the AP reflects fewer signals and is less effective in affecting signal distribution.

**Reflector Size.** We also study the impact of reflector size on reflector’s ability to adjust signal distribution. A larger reflector reflects more signals and can be more effective, however its fabrication is harder and more costly. We aim to seek a proper size to achieve a good tradeoff. We fabricate the reflector in two sizes: 20 cm × 20 cm and 40 cm × 40 cm. Given that the height and width of all our APs are roughly 20 cm, a 20 cm × 20 cm reflector can cover all antennas. We place each reflector around the AP and measure the resulting RSS change at room1 and room2. As we compare the mean RSS change and
Figure 5.8: Accuracy of 3D wireless propagation modeling, in comparison to the 2D modeling in prior work (15).

the standard deviation for these two sizes, we observe negligible difference, indicating as long as the reflector covers all antennas, it needs not to be larger. This observation can be a guideline for determining reflector size for APs in other sizes.

5.5 Microbenchmarks

Finally, we compare the impact of different metal materials on wireless signals, we also examine the accuracy of our 3D wireless modeling and overall running time of the shape optimization.

Material Comparison. To determine the metal material, we systematically test three types of metal sheets made of silver, copper, and aluminum, which are all 0.1-mm thick. We also test aluminum sheet with 0.25-mm thickness to evaluate the impact of the metal-layer thickness. We attach each metal sheet to a 30 cm × 30 cm plastic (the same material used by 3D printers in fabrication) to form the final reflector. We place the reflector at the back of an AP to test its ability to reflect Wi-Fi signals to a receiver. To test its ability to attenuate signals, we place the reflector between the AP and the receiver. For both tests, we vary the distance of the receiver to the AP from 1 m to 3 m.

In Figure 5.9, we see that copper and aluminum perform similarly in enhancing and
Figure 5.9: Different plane reflector’s ability to reflect and attenuate Wi-Fi signals, at distances from 1 to 3 meters.

attenuating Wi-Fi signals, and silver performs slightly better. Increasing sheet thickness moderately improves its ability to attenuate signals, but not its reflection property. Given the lower cost of aluminum and the difficulty of applying a 0.1-mm sheet to an uneven reflector surface, we choose to cover the reflector surface with a 0.024-mm household aluminum foil.

We also observe that reflectors are better at weakening than strengthening Wi-Fi signals, mainly because of Wi-Fi’s wavelength and the energy loss when signals penetrate the reflector. When Wi-Fi signals interact with the reflector, the signal either penetrates, or is absorbed, or is reflected by the reflector. Only the reflected energy can be directed to strengthen the signal at locations before the reflector, while both the reflected and the absorbed energy contribute to the signal attenuation at locations behind the reflector.

Accuracy of 3D Wireless Modeling. Using scene 1 as an example, Figure 5.8 (a) and (b) plot CDFs of absolute RSS errors of our 3D wireless model, using measured RSS as ground truth. Figure 5.8 (a) is the result without any reflector, while Figure 5.8 (b) is for a concave shaped reflector placed around the AP. Overall the mean RSS error of 3D wireless modeling is 3 dBm.

Furthermore, we compare our 3D modeling to the 2D modeling in a prior work (15). We observe that 3D modeling notably lowers the tail of RSS errors. The maximal error
Figure 5.10: Our shape optimization algorithm stabilizes at an optimized shape within 0.5 hr (a). Our speedup schemes (Kd-Tree and multiple threads) reduce the running time of each iteration from 9.78 s to 1.71 s (b).

of 2D modeling is 11 dBm and 16 dBm, with and without reflector respectively, while they are 8 dBm and 12 dBm for 3D modeling. 3D modeling outperforms 2D modeling because of more accurate characterization of signal interaction in the third dimension. We also include the results when 2D/3D wireless modeling uses a finer-grained environment model that includes main furniture (e.g., desks, sofas). We observe that for both 2D and 3D modeling, adding furniture leads to negligible difference in resulting accuracy in both scenarios. The results indicate that coarse-grained 3D environmental models are sufficient.

Running Time. We run our shape optimization algorithm on a MacBook Pro (2.2 GHz Intel Core i7) and record the time to generate an optimized shape for various target coverage requirements. Figure 5.10(a) compares how the objective function (Eq. (3.3)) decreases using our algorithm with the standard SA. They allow the addition of gradient computation to improve the optimized shape with minor increase in the running time. We observe that the algorithm stabilizes after 23 minutes on average.

We further look into effectiveness of our speedup schemes: the Kd-tree used to speed up wireless modeling, the SPSA algorithm and multiple threads to speed up the search for optimized shape. Figure 5.10(b) lists the running time of the optimization process when using either no speedup scheme, or only one speedup scheme, or all of them. Having 107 triangle meshes and 10K rays in the ray tracing model, we see that the Kd-tree ac-
celerate around 1.6 times. For a complex model that has thousands of triangle meshes, the speedup of Kd-tree can be up to tens of times. Theoretically SPSA can reduce tens of time to calculate the gradient when we have $3 \times 5$ control points, however it only speeds up roughly 1.5 times, because the search for appropriate step size is another bottleneck. Multiple threads accelerate nearly 4 times. Together, they reduce the average running time from 207 minutes to 23 minutes.
Chapter 6

Conclusion

In this paper, we sought a different approach to controlling wireless signal propagation for a given environment without needing directional antennas. We studied the design of a low-cost, 3D-fabricated reflector to customize wireless coverage. We present a systematic approach of computing fine details of the reflector shape to achieve a rich set of signal distributions given a indoor environment. We physically fabricated the reflector using 3D digital manufacturing (“3D printing”) and demonstrated the efficacy of optimized reflectors with reflector prototypes and indoor experiments. We evaluated their effectiveness using measurements in two indoor scenarios. We programmed a drone to automate wireless measurements in the 3D space and examined the resulting signal distribution after placing the optimized reflector. We further measured the wireless throughput to examine the actual performance gain experienced by end users. We also tested the impact of placement of the reflector, the accuracy of our 3D wireless propagation model, and computational cost of optimization method.

We obtain the following key findings. Our system only takes 23 minutes to compute an optimized reflector. Our optimized reflectors effectively steer the Wi-Fi signals towards target wireless coverages. It results in up to 10 dB signal enhancement or decline in
areas where users desire stronger or weaker Wi-Fi signals, which translates into 63.3% throughput differences experienced by end users. The optimized reflector is relatively easy to place. Its efficacy is not sensitive to slight placement offsets, tolerating up to $10^\circ$ offset in orientation and 10 cm offset in the distance to the AP. It is also applicable to various Wi-Fi APs including MIMO APs. It offers better flexibility in controlling the Wi-Fi coverage and coexist with the high-end, costly AP with directional antennas. This work has been published at BuildSys’17 conference and covered by a wide range of medias (72). Its related YouTube video got over 0.6 million views (4).

6.1 Limitations and Future Work

We summarize the limitations of our current study and elaborate our plan for future work.

**Application to higher frequency bands.** While we use Wi-Fi as a case study in this work, our approach is applicable to other frequency bands such as millimeter waves and visible light spectrum. In addition, the wavelength of Wi-Fi signals limits reflector’s ability to reflect and block signals (Figure 5.9). Thus, changes on RSS and throughput have been moderate. Moving forward, we will examine higher frequency bands such as millimeter waves and visible light, where reflectors can block and reflect signals more effectively and cause more significant change in signal distribution. Generalizing to other frequency bands only requires to adapt the 3D wireless modeling to best capture the propagation behaviors on those bands. The same shape optimization procedure can be applied to identify the 3D reflector shape.

**Diverse and dynamic indoor scenarios.** We plan to test more diverse indoor scenarios and examine the efficacy of our approach. For the simplicity and feasibility of the user input, we assumed the same material for objects in the environment. To consider hetero-
geneous materials, we can adapt the reflection, transmission and diffraction coefficients in Eq. (4.2) based on materials, and track what materials a ray has traveled through. We will also more thoroughly evaluate the impact of moving users on the reflector’s ability to affect the signal distribution.

**Advanced materials.** After we fabricate the reflector, we cover the reflector with a thin aluminum foil. The aluminum foil crumples a lot and the wrinkles in the sheet might have unpredictable influence on the RF waves, thus in the future we may consider metal electroplating our reflector. We plan to apply metal electroplating to coat the reflector with a thin layer of aluminum or copper. It is low-cost (e.g., <$35 for a 20 cm × 20 cm area). It produces a wrinkle-free surface, potentially improving the effectiveness of fabricated reflectors. On the other hand, the efficacy is limited by Wi-Fi signal’s ability of penetrating the reflector, marginal enhancement at signal level, we hope in the future we can use more advanced materials that has higher impact on the signals to fabricate the reflector.

**Transformable reflector.** Since our current study focuses on a static reflector, upon any substantial environment changes (e.g., removal/addition of walls), users need to input the updated environment setup and fabricate a new reflector to achieve the target coverage. In the future, we plan to study reflectors made of transformable materials, enabling the reflector to automatically adapt its shape upon major changes.
Bibliography


